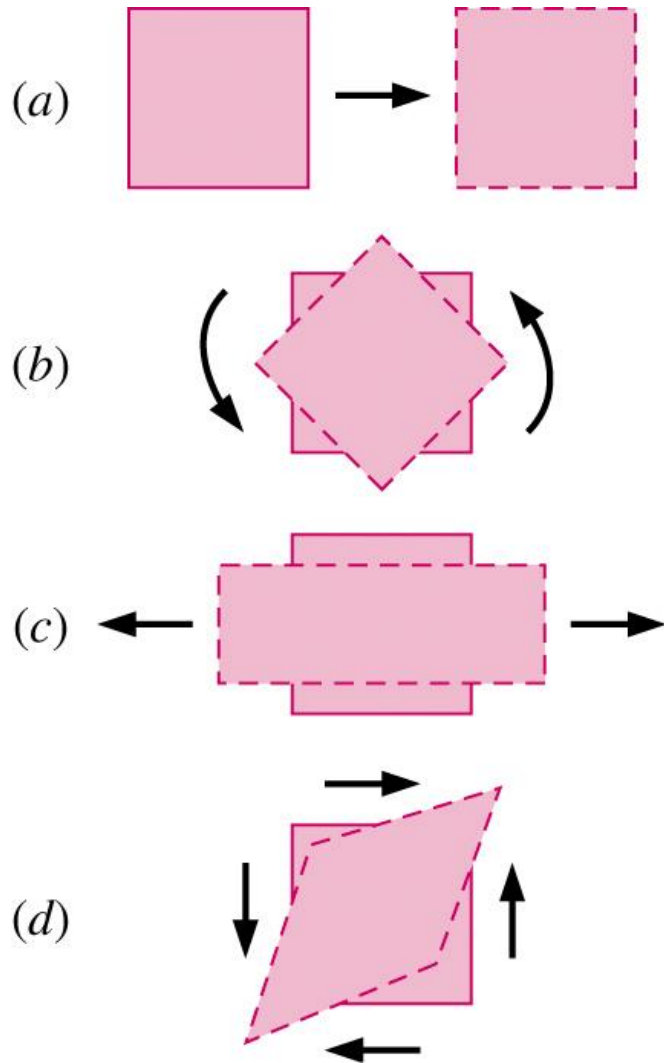


Kinematic Description



- In fluid mechanics, an element may undergo four fundamental types of motion.
 - a) Translation
 - b) Rotation
 - c) Linear strain
 - d) Shear strain
- Because fluids are in constant motion and deformation, they are better described in terms of rates
 - a) velocity: rate of translation
 - b) angular velocity: rate of rotation
 - c) linear strain rate: rate of linear strain
 - d) shear strain rate: rate of shear strain

Rate of Translation and Rotation

- To be useful, these rates must be expressed in terms of velocity and derivatives of velocity
- The **rate of translation vector** is described as the velocity vector. In Cartesian coordinates:

$$\vec{V} = u\vec{i} + v\vec{j} + w\vec{k}$$

(Handwritten red annotations: u_x under u , u_y under v , u_z under w)

- **Rate of rotation** at a point is defined as the average rotation rate of two initially perpendicular lines that intersect at that point.

The rate of rotation vector in Cartesian coordinates:

$$\vec{\omega} = \vec{\omega} \times \vec{v}$$

(Handwritten red equation)

$$\vec{\omega} = \frac{1}{2} \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \vec{i} + \frac{1}{2} \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \vec{j} + \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \vec{k}$$

$$= \frac{1}{2} \nabla \times \vec{v}$$

(Handwritten red equation in a box)

Tabela com o operador del em coordenadas cartesianas, cilíndricas e esféricas

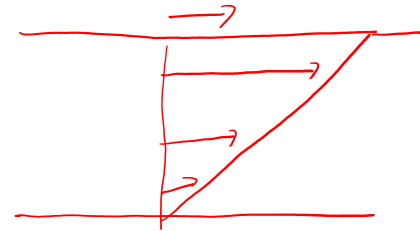
Operação	Coordenadas cartesianas (x, y, z)	Coordenadas cilíndricas (ρ, φ, z)	Coordenadas esféricas (r, θ, φ), onde φ é o polar e θ é o ângulo azimutal °
campo vetorial A	$A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$	$A_\rho \hat{\rho} + A_\varphi \hat{\varphi} + A_z \hat{z}$	$A_r \hat{r} + A_\theta \hat{\theta} + A_\varphi \hat{\varphi}$
Gradiente ∇f	$\frac{\partial f}{\partial x} \hat{x} + \frac{\partial f}{\partial y} \hat{y} + \frac{\partial f}{\partial z} \hat{z}$	$\frac{\partial f}{\partial \rho} \hat{\rho} + \frac{1}{\rho} \frac{\partial f}{\partial \varphi} \hat{\varphi} + \frac{\partial f}{\partial z} \hat{z}$	$\frac{\partial f}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial f}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial f}{\partial \varphi} \hat{\varphi}$
Divergência ∇ · A	$\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$	$\frac{1}{\rho} \frac{\partial (\rho A_\rho)}{\partial \rho} + \frac{1}{\rho} \frac{\partial A_\varphi}{\partial \varphi} + \frac{\partial A_z}{\partial z}$	$\frac{1}{r^2} \frac{\partial (r^2 A_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial A_\varphi}{\partial \varphi}$
Rotacional ∇ × A	$\left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \hat{x}$ + $\left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) \hat{y}$ + $\left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \hat{z}$	$\left(\frac{1}{\rho} \frac{\partial A_z}{\partial \varphi} - \frac{\partial A_\varphi}{\partial z} \right) \hat{\rho}$ + $\left(\frac{\partial A_\rho}{\partial z} - \frac{\partial A_z}{\partial \rho} \right) \hat{\varphi}$ + $\frac{1}{\rho} \left(\frac{\partial (\rho A_\varphi)}{\partial \rho} - \frac{\partial A_\rho}{\partial \varphi} \right) \hat{z}$	$\frac{1}{r \sin \theta} \left(\frac{\partial}{\partial \theta} (A_\varphi \sin \theta) - \frac{\partial A_\theta}{\partial \varphi} \right) \hat{r}$ + $\frac{1}{r} \left(\frac{1}{\sin \theta} \frac{\partial A_r}{\partial \varphi} - \frac{\partial}{\partial r} (r A_\varphi) \right) \hat{\theta}$ + $\frac{1}{r} \left(\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \hat{\varphi}$
Operador de Laplace ∇²f ≡ Δf	$\frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2}$	$\frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \varphi^2} + \frac{\partial^2 f}{\partial z^2}$	$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 f}{\partial \varphi^2}$
Vetor de Laplace ∇²A ≡ ΔA	$\nabla^2 A_x \hat{x} + \nabla^2 A_y \hat{y} + \nabla^2 A_z \hat{z}$	$\left(\nabla^2 A_\rho - \frac{A_\rho}{\rho^2} - \frac{2}{\rho^2} \frac{\partial A_\varphi}{\partial \varphi} \right) \hat{\rho}$ + $\left(\nabla^2 A_\varphi - \frac{A_\varphi}{\rho^2} + \frac{2}{\rho^2} \frac{\partial A_\rho}{\partial \varphi} \right) \hat{\varphi}$ + $\nabla^2 A_z \hat{z}$	$\left(\nabla^2 A_r - \frac{2A_r}{r^2} - \frac{2}{r^2 \sin \theta} \frac{\partial (A_\theta \sin \theta)}{\partial \theta} - \frac{2}{r^2 \sin \theta} \frac{\partial A_\varphi}{\partial \varphi} \right) \hat{r}$ + $\left(\nabla^2 A_\theta - \frac{A_\theta}{r^2 \sin^2 \theta} + \frac{2}{r^2} \frac{\partial A_r}{\partial \theta} - \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial A_\varphi}{\partial \varphi} \right) \hat{\theta}$ + $\left(\nabla^2 A_\varphi - \frac{A_\varphi}{r^2 \sin^2 \theta} + \frac{2}{r^2 \sin \theta} \frac{\partial A_r}{\partial \varphi} + \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial A_\theta}{\partial \varphi} \right) \hat{\varphi}$

Linear Strain Rate

$$\epsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

- **Linear Strain Rate** is defined as the rate of increase in length per unit length.
- In Cartesian coordinates

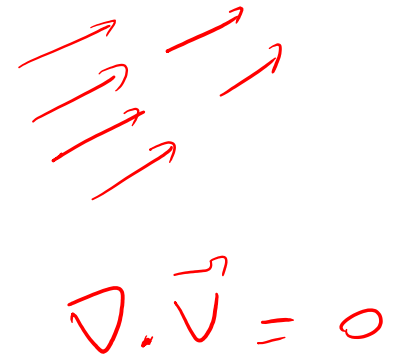
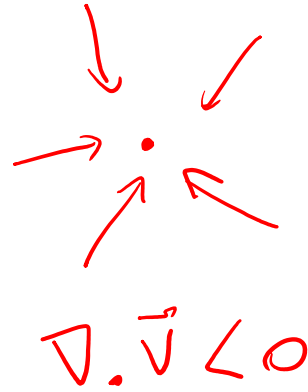
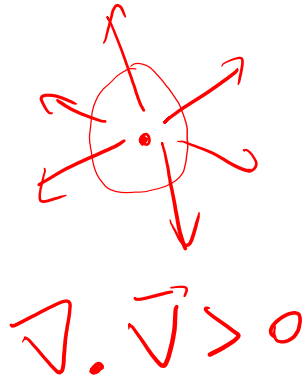
$$\epsilon_{xx} = \frac{\partial u}{\partial x}, \epsilon_{yy} = \frac{\partial v}{\partial y}, \epsilon_{zz} = \frac{\partial w}{\partial z}$$



- Volumetric strain rate in Cartesian coordinates

$$\frac{1}{V} \frac{DV}{Dt} = \epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = \nabla \cdot \vec{v}$$

- Since the volume of a fluid element is constant for an incompressible flow, the volumetric strain rate must be zero.



$$\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad (\text{Analogie: Lei de Gauss})$$

Shear Strain Rate

- **Shear Strain Rate** at a point is defined as *half of the rate of decrease of the angle between two initially perpendicular lines that intersect at a point.*
- Shear strain rate can be expressed in Cartesian coordinates as:

$$\varepsilon_{xy} = \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right), \varepsilon_{zx} = \frac{1}{2} \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right), \varepsilon_{yz} = \frac{1}{2} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)$$

Shear Strain Rate

We can combine linear strain rate and shear strain rate into one symmetric second-order tensor called the **strain-rate tensor**.

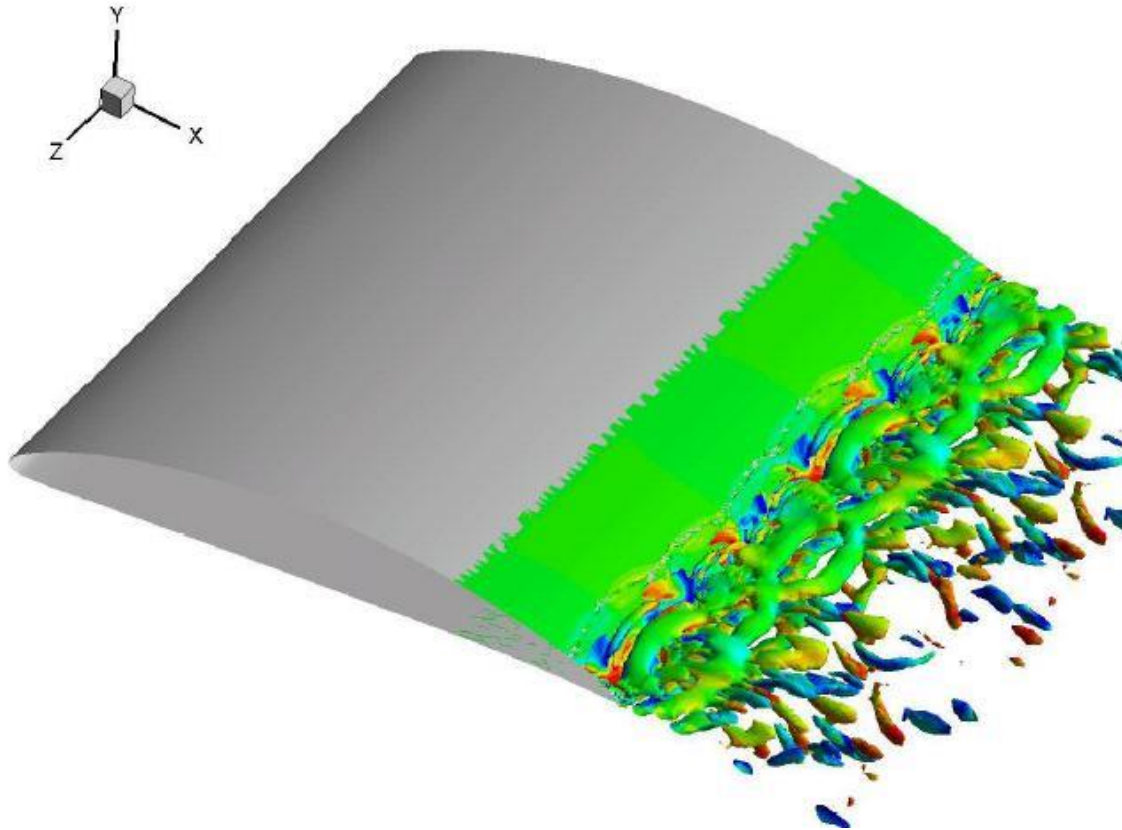
$$\boldsymbol{\varepsilon}_{ij} = \begin{pmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \\ \varepsilon_{yx} & \varepsilon_{yy} & \varepsilon_{yz} \\ \varepsilon_{zx} & \varepsilon_{zy} & \varepsilon_{zz} \end{pmatrix} = \begin{pmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \\ \frac{1}{2} \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) & \frac{\partial v}{\partial y} & \frac{1}{2} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \\ \frac{1}{2} \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) & \frac{1}{2} \left(\frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) & \frac{\partial w}{\partial z} \end{pmatrix}$$

Shear Strain Rate

- Purpose of our discussion of fluid element kinematics:
 - Better appreciation of the inherent complexity of fluid dynamics
 - Mathematical sophistication required to fully describe fluid motion
- Strain-rate tensor is important for numerous reasons. For example,
 - Develop relationships between fluid stress and strain rate.
 - Feature extraction and flow visualization in CFD simulations.

Shear Strain Rate

Example: Visualization of trailing-edge turbulent eddies for a hydrofoil with a beveled trailing edge



Feature extraction method is based upon eigen-analysis of the strain-rate tensor.

Vorticity and Rotationality

- The **vorticity vector** is defined as the curl of the velocity vector

$$\vec{\zeta} = \vec{\nabla} \times \vec{V}$$

- Vorticity is equal to twice the angular velocity of a fluid particle.

$$\vec{\zeta} = 2\vec{\omega}$$

Cartesian coordinates

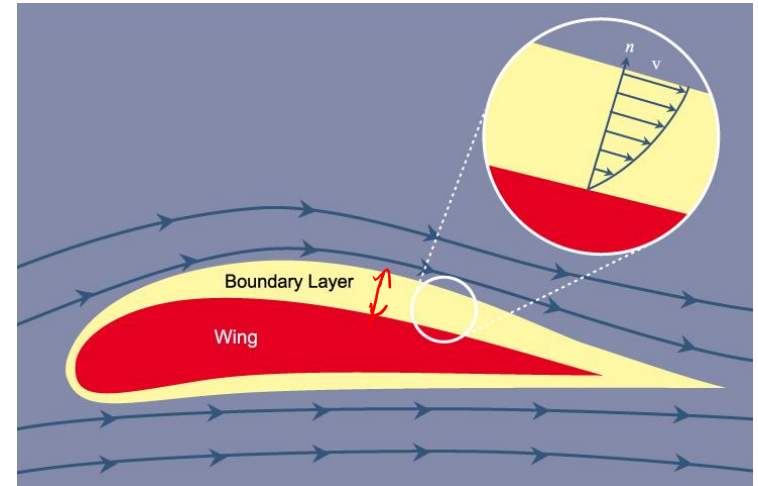
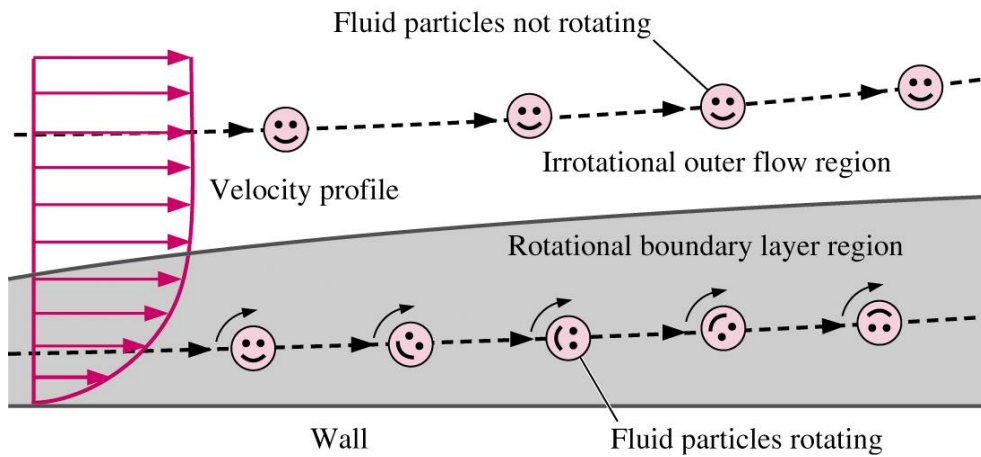
$$\vec{\zeta} = \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \vec{i} + \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \vec{j} + \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \vec{k}$$

Cylindrical coordinates

$$\vec{\zeta} = \left(\frac{1}{r} \frac{\partial u_z}{\partial \theta} - \frac{\partial u_\theta}{\partial z} \right) \vec{e}_r + \left(\frac{\partial u_r}{\partial z} - \frac{\partial u_z}{\partial r} \right) \vec{e}_\theta + \left(\frac{\partial(ru_\theta)}{\partial r} - \frac{\partial u_r}{\partial \theta} \right) \vec{e}_z$$

- In regions where $\zeta = 0$, the flow is called **irrotational**.
- Elsewhere, the flow is called **rotational**.

Vorticity and Rotationality

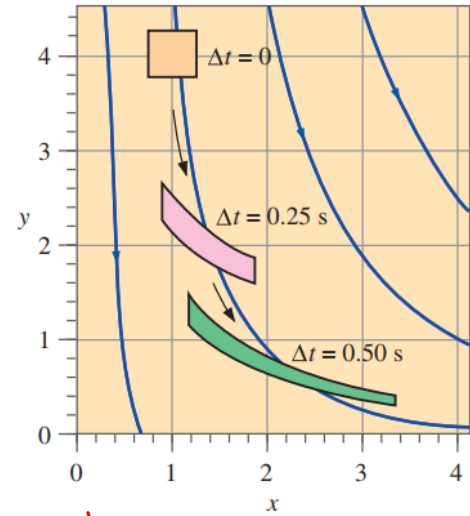


EXAMPLE 4-8 **Determination of Rotationality
in a Two-Dimensional Flow**

Consider the following steady, incompressible, two-dimensional velocity field:

$$\vec{V} = (u, v) = x^2 \vec{i} + (-2xy - 1) \vec{j} \quad (1)$$

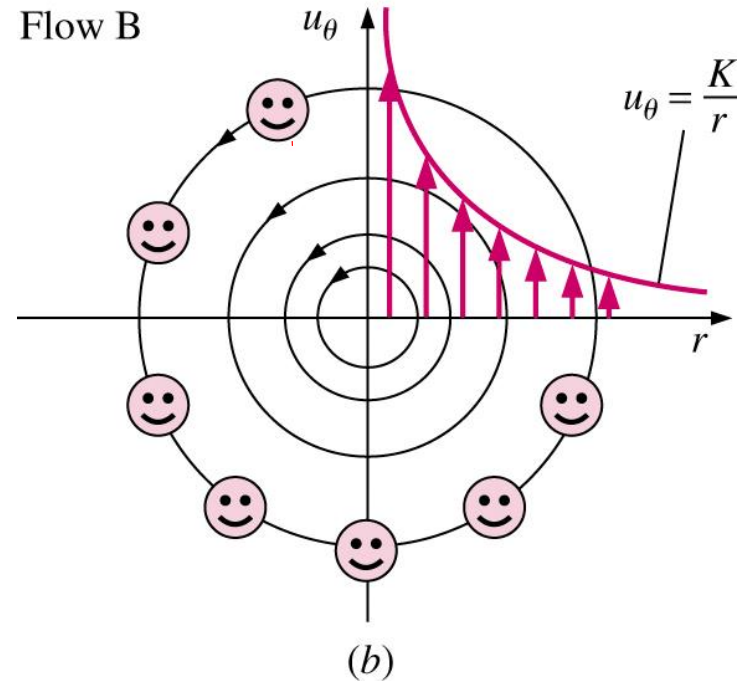
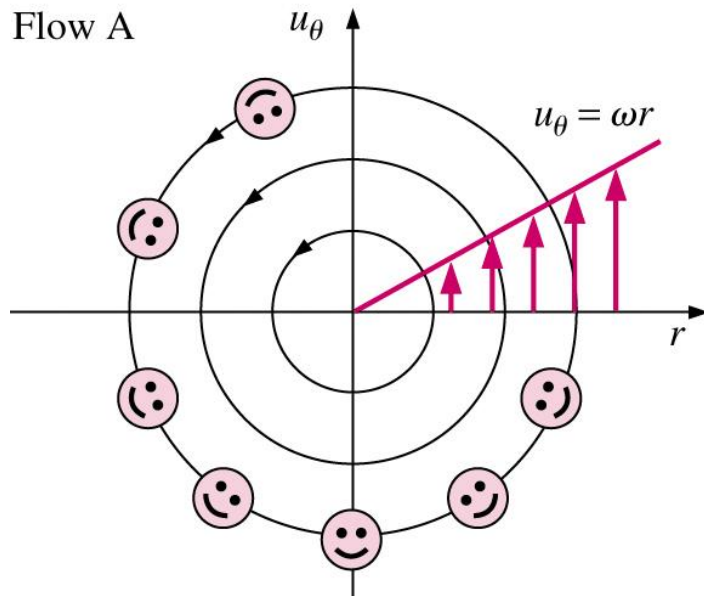
Is this flow rotational or irrotational? Sketch some streamlines in the first quadrant and discuss.



$$\vec{\zeta} = \nabla \times \vec{V} = \hat{z} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) = \hat{z} \left(-2y - \frac{\partial}{\partial y} (x^2) \right) = -2y \hat{z}$$

Comparison of Two Circular Flows

Special case: consider two flows with circular streamlines



$$u_r = 0, u_\theta = \omega r$$

$$\vec{\zeta} = \frac{1}{r} \left(\frac{\partial(ru_\theta)}{\partial r} - \frac{\partial u_r}{\partial \theta} \right) \vec{e}_z = \frac{1}{r} \left(\frac{\partial(\omega r^2)}{\partial r} - 0 \right) \vec{e}_z = 2\omega \vec{e}_z$$

$$u_r = 0, u_\theta = \frac{K}{r}$$

$$\vec{\zeta} = \frac{1}{r} \left(\frac{\partial(ru_\theta)}{\partial r} - \frac{\partial u_r}{\partial \theta} \right) \vec{e}_z = \frac{1}{r} \left(\frac{\partial(K)}{\partial r} - 0 \right) \vec{e}_z = 0 \vec{e}_z$$